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# LOD-BOR-FDTD Algorithm for Efficient Analysis of Circularly Symmetric Structures

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Abstract—The unconditionally stable locally 1-D (LOD) scheme is used to develop an efficient implicit body-of-revolution (BOR) finite-difference time-domain (FDTD) method. In the LOD-BOR-FDTD, the number of arithmetic operations of the resultant finite-difference equations is significantly reduced, when compared with the alternating-direction implicit (ADI) BOR-FDTD. Numerical results of circular cavity resonators reveal that the LOD-BOR-FDTD provides resonance frequencies identical to the ADI counterparts, with the computational time being reduced to 70%.

Index Terms—Body of revolution (BOR), locally 1-D finite-difference time-domain method (LOD-FDTD), rotationally symmetric geometry, unconditional stability.

#### I. INTRODUCTION

HE body-of-revolution finite-difference time-domain (BOR-FDTD) method [1]–[3] is an effective means for treating electromagnetic problems of circularly symmetric structures. Note, however, that as in the conventional FDTD a time step size of the BOR-FDTD is limited by the Courant-Friedrich-Levy (CFL) condition. This limitation has been removed [4] using the alternating-direction implicit (ADI) scheme [5], [6]. Recently, the weakly conditionally stable scheme [7] has been applied to the BOR-FDTD [8], in which the time step size is subject to only single space discretization.

On the other hand, the locally 1-D (LOD) scheme has been introduced to the unconditionally stable implicit FDTD formulation [9]–[11]. The LOD-FDTD provides a quite simple algorithm compared with the ADI algorithm. Strictly speaking, the LOD formulation is a simple type of split-step approach [12] and is first-order accurate in time [11], whereas the ADI formulation is second-order accurate in time. Nevertheless, the numerical results obtained from the LOD-FDTD have been found to be comparable to the ADI counterparts for not only the 2-D [9], [11], [13] but also 3-D problems [14]-[16]. Therefore, the LOD-FDTD could be a practical alternative for an efficient implicit FDTD. This letter is devoted to the application of the LOD scheme to the BOR-FDTD for efficient implicit calculations of circularly symmetric structures. The usefulness of the LOD-BOR-FDTD is investigated through the analysis of circular cavity resonators with and without a dielectric disc, along with the explicit BOR-FDTD and ADI-BOR-FDTD.

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#### II. FORMULATION

In the circularly symmetric structures, the fields can be expanded in a Fourier series of sines and cosines as [1]

$$E = \sum_{\substack{m=0\\ \infty}}^{\infty} (E_{\text{even},m} \cos m\phi + E_{\text{odd},m} \sin m\phi)$$
 (1a)

$$H = \sum_{m=0}^{\infty} (H_{\text{even},m} \cos m\phi + H_{\text{odd},m} \sin m\phi)$$
 (1b)

where m is the mode number. Substituting (1) into Maxwell's equations in cylindrical coordinates, we obtain the following equation in the matrix form:

$$\frac{\partial \boldsymbol{u}}{\partial t} = ([A] + [B])\boldsymbol{u} \tag{2}$$

where  $\boldsymbol{u} = [E_{\rho}, E_{\phi}, E_z, H_{\rho}, H_{\phi}, H_z]^T$  and

$$[A] = \begin{bmatrix} 0 & 0 & 0 & 0 & -\frac{\partial}{\epsilon\partial z} & 0\\ 0 & 0 & 0 & 0 & 0 & -\frac{\partial}{\epsilon\partial\rho}\\ 0 & 0 & 0 & -\frac{m}{\epsilon\rho} & 0 & 0\\ 0 & 0 & \frac{m}{\mu\rho} & 0 & 0 & 0\\ -\frac{\partial}{\mu\partial z} & 0 & 0 & 0 & 0 & 0\\ 0 & -\frac{\partial(\rho)}{\mu\rho\partial\rho} & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$[B] = \begin{bmatrix} 0 & 0 & 0 & 0 & \frac{m}{\epsilon\rho}\\ 0 & 0 & 0 & \frac{\partial}{\epsilon\partial z} & 0 & 0\\ 0 & 0 & 0 & \frac{\partial}{\epsilon\partial z} & 0 & 0\\ 0 & \frac{\partial}{\mu\partial z} & 0 & 0 & 0 & 0\\ 0 & 0 & \frac{\partial}{\mu\partial\rho} & 0 & 0 & 0\\ -\frac{m}{\mu\rho} & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

in which  $\epsilon$  and  $\mu$  represent permittivity and permeability, respectively. Applying the Crank–Nicolson scheme to (2) gives

$$u^{n+1} = \frac{[I] + \frac{\Delta t}{2}([A] + [B])}{[I] - \frac{\Delta t}{2}([A] + [B])} u^n$$
 (3)

where I denotes the unit matrix. We discretize (3) using the LOD scheme, so that

$$\boldsymbol{u}^{n+1/2} = \frac{[I] + \frac{\Delta t}{2}[B]}{[I] - \frac{\Delta t}{2}[B]} \boldsymbol{u}^n$$
 (4a)

for the first step and

$$\mathbf{u}^{n+1} = \frac{[I] + \frac{\Delta t}{2}[A]}{[I] - \frac{\Delta t}{2}[A]} \mathbf{u}^{n+1/2}$$
 (4b)

for the second step.

TABLE I
NUMBER OF ARITHMETIC OPERATIONS

Method	Implicit		Explicit		Total	
	M/D	A/S	M/D	A/S	M/D	A/S
ADI	12	20	13	20	25	40
LOD	11	16	5	16	16	32

For simplicity, we will examine the case for m=0, so that the LOD-BOR-FDTD equations are derived as

$$E_{\rho}^{n+1/2} = E_{\rho}^n \tag{5a}$$

$$E_{\phi}^{n+1/2} - \frac{\Delta t}{2\epsilon} \frac{\partial H_{\rho}^{n+1/2}}{\partial z} = E_{\phi}^{n} + \frac{\Delta t}{2\epsilon} \frac{\partial H_{\rho}^{n}}{\partial z}$$
 (5b)

$$E_z^{n+1/2} - \frac{\Delta t}{2\epsilon\rho} \frac{\partial (\rho H_\phi^{n+1/2})}{\partial \rho} = E_z^n + \frac{\Delta t}{2\epsilon\rho} \frac{\partial (\rho H_\phi^n)}{\partial \rho} \quad (5c)$$

$$H_{\rho}^{n+1/2} - \frac{\Delta t}{2\mu} \frac{\partial E_{\phi}^{n+1/2}}{\partial z} = H_{\rho}^{n} + \frac{\Delta t}{2\mu} \frac{\partial E_{\phi}^{n}}{\partial z}$$
 (5d)

$$H_{\phi}^{n+1/2} - \frac{\Delta t}{2\mu} \frac{\partial E_z^{n+1/2}}{\partial \rho} = H_{\phi}^n + \frac{\Delta t}{2\mu} \frac{\partial E_z^n}{\partial \rho}$$
 (5e)

$$H_z^{n+1/2} = H_z^n \tag{5f}$$

for the first step and

$$E_{\rho}^{n+1} + \frac{\Delta t}{2\epsilon} \frac{\partial H_{\phi}^{n+1}}{\partial z} = E_{\rho}^{n+1/2} - \frac{\Delta t}{2\epsilon} \frac{\partial H_{\phi}^{n+1/2}}{\partial z}$$
 (6a)

$$E_{\phi}^{n+1} + \frac{\Delta t}{2\epsilon} \frac{\partial H_z^{n+1}}{\partial \rho} = E_{\phi}^{n+1/2} - \frac{\Delta t}{2\epsilon} \frac{\partial H_z^{n+1/2}}{\partial \rho}$$
(6b)
$$E_z^{n+1} = E_z^{n+1/2}$$
(6c)
$$H_{\rho}^{n+1} = H_{\rho}^{n+1/2}$$
(6d)

$$E_z^{n+1} = E_z^{n+1/2} (6c)$$

$$H_{\rho}^{n+1} = H_{\rho}^{n+1/2} \tag{6d}$$

$$H_{\phi}^{n+1} + \frac{\Delta t}{2\mu} \frac{\partial E_{\rho}^{n+1}}{\partial z} = H_{\phi}^{n+1/2} - \frac{\Delta t}{2\mu} \frac{\partial E_{\rho}^{n+1/2}}{\partial z} \tag{6e}$$

$$H_z^{n+1} + \frac{\Delta t}{2\mu\rho} \frac{\partial \left(\rho E_\phi^{n+1}\right)}{\partial \rho} = H_z^{n+1/2} - \frac{\Delta t}{2\mu\rho} \frac{\partial \left(\rho E_\phi^{n+1/2}\right)}{\partial \rho}$$
(6f)

for the second step. For m=0, we must pay attention to handling the singular point at  $\rho = 0$ . Instead of (5c), we adopt the following equation in accordance with LOD implementation:

$$E_z^{n+1/2} = E_z^n + \frac{4\Delta t}{\epsilon \Delta \rho} H_\phi^{n+1/2}.$$

Now, we solve the above equations. For the TE mode in which the  $E_{\phi}, H_{\rho}$  and  $H_{z}$  fields are calculated, we substitute (5d) into (5b) and implicitly solve the resultant tridiagonal system of linear equations for  $E_{\phi}^{n+1/2}$ , and then explicitly solve (5d) for  $H_{\rho}^{n+1/2}$ . Next, we substitute (6f) into (6b) and implicitly solve the resultant tridiagonal system for  $E_{\phi}^{n+1}$ , and then explicitly solve (6f) for  $H_z^{n+1}$ . The equations for the TM mode can similarly be solved for the  $H_{\phi}, E_{\rho}$  and  $E_z$  fields.

Here, we count the number of arithmetic operations of the right-hand side of the resultant finite-difference equations for

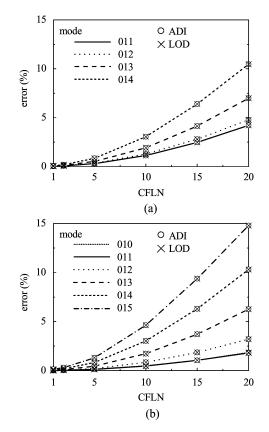


Fig. 1. Error of the resonance frequency versus CFLN. In (b), the errors of the  $TM_{010}$  mode are almost superimposed onto those of the  $TM_{011}$  mode. (a) TE mode, (b) TM mode.

m=0, in comparison with the ADI counterparts. Table I summarizes the results, in which M/D and A/S indicate multiplication/division and addition/subtraction operations, respectively. It is clear that the number for the LOD case is reduced when compared with the ADI case. A reduction becomes significant for  $m \neq 0$ : M/D and A/S are, respectively, 22 and 38 in total for the LOD, while they are 40 and 56 for the ADI. As a result, the algorithm can simply be implemented with the LOD scheme.

#### III. NUMERICAL RESULTS

To assess the LOD-BOR-FDTD in terms of accuracy and efficiency, we analyze the two circular cavity resonators frequently used as a benchmark [3], [4], [17]. The first example is the circular cavity formed by closing the two ends of the waveguide with plates [18], [19]. The radius and height of the cavity are 3.995 cm and 7.910 cm, respectively. The sampling widths are  $\Delta \rho = 0.799$  mm and  $\Delta z = 0.791$  mm. We follow the calculation parameters used in [4], in which a Gaussian pulse with frequency content up to 6 GHz is excited.

Figs. 1(a) and (b) show the errors of the resonance frequencies for the TE and TM modes, respectively, versus time step size CFLN defined by  $\Delta t/\Delta t_{\rm CFL}$  where  $\Delta t_{\rm CFL}=1.3183$  ps is determined by the CFL condition. The theoretical values of the resonance frequencies are available from [18], [19] (our careful calculation reveals that the resonance frequency of the  $TE_{011}$ mode is 4.953 GHz, whereas it is denoted as 4.950 GHz in [4], [17]). The higher-order modes are also investigated. It is found

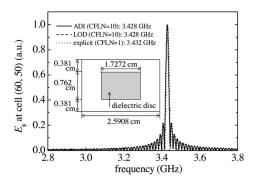


Fig. 2.  $E_{\phi}$  versus frequency. The inset shows a cavity resonator to be studied. The LOD result is almost superimposed onto the ADI result.

that the results of the LOD-BOR-FDTD are in agreement with those of the ADI-BOR-FDTD, in which the error increases with CFLN due to the numerical dispersion. In addition, as the mode becomes higher the error increases, which is caused by a steeper variation of the mode shape. Although not illustrated, the error of the explicit BOR-FDTD for CFLN = 1, relative to the theoretical value, is always less than 0.1% in this example. We here mention the efficiency of the LOD-BOR-FDTD. The computational times, e.g., for CFLN = 10, are 12.3 s and 17.5 s for the LOD- and ADI-BOR-FDTDs, respectively, while the time is 42.7 s for the explicit BOR-FDTD, where a PC with a Pentium 4 processor (3.8 GHz) is utilized. This indicates the time reductions to 70% and 30% of the ADI and explicit counterparts, respectively.

The second example is the circular cavity with the dielectric disc ( $\epsilon_r=35.74$ ) being centered in the cavity [4], [17] (the inset in Fig. 2). The sampling widths are  $\Delta\rho=0.17272$  mm and  $\Delta z=0.1524$  mm. Fig. 2 shows the strength of  $E_\phi$  versus frequency, in which CFLN = 10 is used for the LOD- and ADI-BOR-FDTDs. Again, we can find excellent agreement between the LOD and ADI results, yielding the identical resonance frequency. Although these results slightly deviate from the explicit result (dotted line), the difference in resonance frequency is only 0.12%. We also obtain the same efficiency improvement for the LOD calculations as that mentioned in the first example.

#### IV. CONCLUSION

The efficient implicit BOR-FDTD has been formulated on the basis of the unconditionally stable LOD scheme. The LOD-BOR-FDTD offers the quite simple algorithm with a subsequent reduction in the computational time, maintaining numerical results identical to the ADI counterparts. The LOD formulation can also be applied to the cylindrical coordinate system [17]. For open region problems, efficient absorbing boundary conditions such as perfectly matched layers [20]–[24] are required, the application of which is left for a future study. Further improvement in efficiency may be anticipated if the LOD is implemented in its fundamental scheme [25].

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